

Transient Stability Improvement using Hybrid Controller Design for STATCOM

P.K.Dhal, C.Christober Asir Rajan

Abstract—This paper proposes a transient stability improvement using hybrid controller design for STATCOM with static synchronous time critical error and better damping system oscillations after a short circuit fault. This article on a STATCOM Control for transient stability improvement has proposed a hybrid system with fuzzy and neural controller to meet with the addition of Lyapunov stability criterion to the ability and conditions as well. The performance is analyzed using digital simulation with (SMIB) with infinite bus.

Index Terms— Fuzzy Logic, Neural Network, lyapunov energy function, STATCOM, transient stability.

I. INTRODUCTION

Recent development in electronics can power up, the interest using these elements as the high voltage network devices has increased. These elements not only in the steady state performance can be improved power systems are, but also its high speed compared to the system against disturbances. The generation of bulk power at remote locations necessitates the use of transmission line to connect generation sites to load centers. With long distance ac power transmission and load growth, active control of reactive power is indispensable to stabilize the power system and to maintain the supply voltage.

The static synchronous compensator (STATCOM) using voltage source inverters has been accepted as a competitive alternative to the conventional static VAR compensator (SVC) using thyristor-controlled reactors STATCOM functions as a synchronous voltage source. It can provide reactive power compensation without the dependence on the ac system voltage. By controlling the reactive power, a STATCOM can stabilize the power system, increase the maximum active power flow and regulate the line voltages. Faster response makes STATCOM suitable for continuous power flow control and power system stability improvement

The interaction between the AC system voltage and the inverter-composed voltage provides the control of the STATCOM var output. When these two voltages are synchronized and have the same amplitude, the active and reactive power outputs are zero. However, if the amplitude of the STATCOM voltage is smaller than that of the system voltage, it produces a current lagging the voltage by 90° and the compensator behaves as a variable capacitive load. The reactive power depends on the voltage amplitude. This amplitude control is done through the leading the STATCOM

voltage, it is possible to charge or discharge the dc capacitor; as a consequence, change the value of the dc voltage and the STATCOM's operational characteristics and the compensator behaves as an inductive load, which reactive value depends on the voltage amplitude. Making the STATCOM voltage higher than the AC system voltage the current will lead the voltage by 90° . In the past few decades, various STATCOM systems have been put into service. In this topology, multiple six-pulse inverters are magnetically coupled through a complex zig-zag transformer. An alternative approach is to use multilevel inverters [1-3], which can eliminate the bulky zig-zag transformer.

In [4], to eliminate unequal duty cycles, the required dc capacitance of each inverter unit is calculated according to the corresponding duty cycle. But in practical application modular design is very difficult. By using proposed method inverter units' fundamental output voltage are equalized. A special gating pattern is used for maintain the dc capacitor charge balance and equalize the current stress of the switching device. Among these various multilevel topologies, the cascaded multilevel inverter can implement a high number of levels with ease. The modular structure and the ease of redundant operation are also advantages.

In STATCOM to balance the dc-link voltages, additional auxiliary inverters were used to exchange the energy among various capacitors. But the disadvantage is high cost and complexity in hardware design. In conventional cascaded multilevel inverter use fundamental switching frequency [5] to generate step waveform at low harmonic distortion and keep the switching loss as low as possible. But the inverter units' duty cycles are different from each other. Due to unequal duty cycle the inverter units cannot equally share the exchanged power with the utility grid [6]. To overcome the limitations of semiconductor device, many new techniques are developed [7-9]. Recently alternate methods [10-12] of implementing these switching patterns have been developed without using real time solution of nonlinear harmonic elimination equation; an ANN is trained off-line to output the switching angles for wanted output voltage. They are multiple switching elements in one leg of an inverter, series connected inverter and parallel connected inverters [13-14]. Fuzzy Control and Dynamic Performance of STATCOM were analysed and found that it was giving better performance than the without controller case. The time critical error was reduced and transient performance was improved [15]. Application of a Fuzzy Controller for Transient Stability Enhancement of AC Transmission System by STATCOM was analysed and found that through the

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P.K.Dhal, Department of EEE, Sathyabama University, Chennai, India, 9884123207, (e-mail: pradvumna.dhal@rediffmail.com).

C.Christober Asir Rajan, Department of EEE, Pondicherry Engineering College, Puducherry, Chennai, 9443713846, (e-mail: asir_70@pec.edu).

transient stability curve and concluded that the transient stability value was reduced in the considered method. But the rules framed are not made through the actual occurrence of a fault [16].

In this paper, the hybrid controller design for creating controller is very effective. This article on a STATCOM Control for transient stability improvement has proposed a hybrid system with fuzzy and neural controller to meet with the addition of Lyapunov stability criterion to the ability and conditions as well.

II. FUNDAMENTAL FREQUENCY MODULATION

A. Cascaded multilevel inverter

Fig. 1 shows the basic structure of cascaded multilevel inverter with separate dc source. For a three phase system, the output voltage of the three cascaded inverters can be connected either star or delta [3].

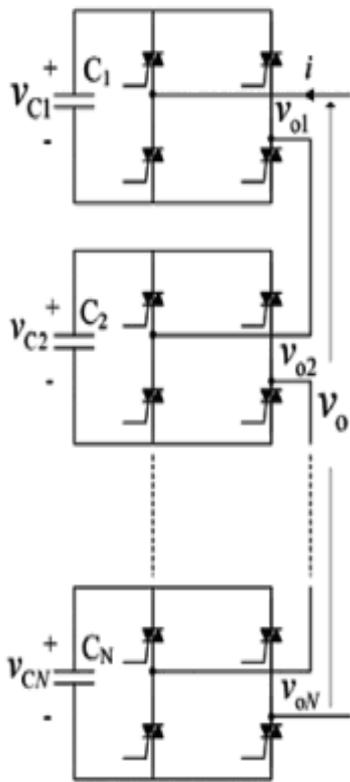


Fig. 1. Basic Structure of Cascaded Multilevel Inverter

III. MULTILEVEL OPTIMAL MODULATION STRATEGY

A. Algorithm of the Multilevel Optimal Modulation

A 100Mvar STATCOM device is connected to the 230-kV (L-L) grid network. Fig. 2 shows the single line diagram representing the STATCOM and the host sample grid network. The feeding network is represented by a Thevenin equivalent at (bus B1) where the voltage source is represented by a kV with 10,000 MVA short circuit power level with a followed by the transmission line connected to bus B2. The STATCOM device comprises the voltage source converter-cascade model connected to the host electric grid. 7-level is chosen here for STATCOM. It is connected to the network through the coupling transformer. The dc link

voltage is provided by the capacitor C, which is charged from the ac network. The decoupled current control system ensures full dynamic regulation of the bus voltage and the dc link voltage.

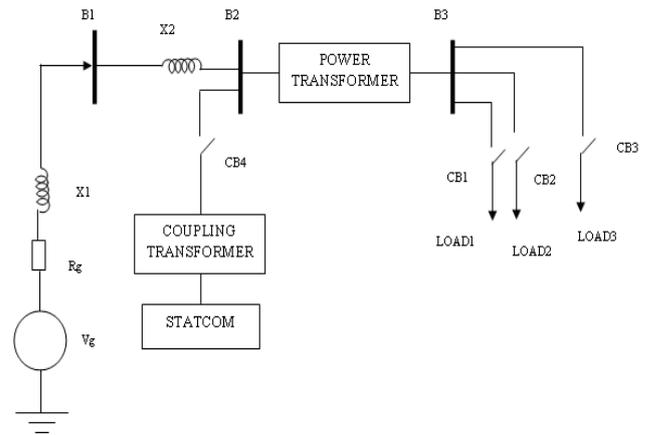


Fig. 2. Single line Diagram representing the STATCOM

At the time of starting the source voltage is such that the STATCOM is inactive. It neither absorbs nor provides reactive power to the network. The following load sequence is tested and results are taken.

At $t=0.06$ sec STATCOM is connected to the system by switching circuit breaker CB4.

At $t=0.1$ load 1 is connected by switching CB1.

At $t=0.3$ load 2 is connected by switching CB2.

At $t=0.5$ load 2 is connected by switching CB3.

STATCOM system is given in the Appendix.

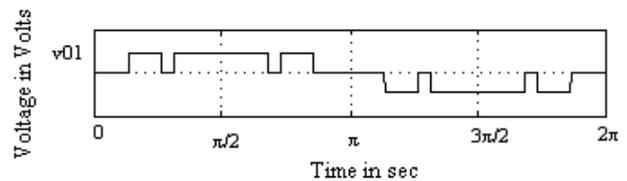


Fig. 3. Waveforms of the output voltages of inverter units and their switching angles

Fig. 3 illustrates the typical output voltage waveforms when using the proposed optimal modulation strategy. The square wave is chopped three times per half cycle and the corresponding switching frequency of the IGBTs is 150Hz. The three switching angles of the inverter unit are depicted using. Since the waveform has quarter-wave and half wave symmetry, not even harmonics exist. And it is normalized with respect to the corresponding dc-link voltage.

Compared with the fundamental frequency technique, a disadvantage of the 150 Hz modulation techniques is the unequal conduction time of the four switching devices in one inverter unit, as illustrated in Fig.4. To realize an equal utilization of the switching devices, a special scheme is developed to swap the gating signals among the four switching devices in an inverter unit. As shown in Fig.3, there are two gating patterns for the inverter unit to generate the desired voltage waveform.

They are denoted as Pattern-1 and Pattern-2. Swapping these two gating

patterns per cycle can equalize the average conduction time of the switching devices and equalize the devices' current stress. However it should be noted that an additional switching action occurs at the swapping time, which brings unexpected increase of switching loss. To minimize this additional switching loss, the gating-pattern is swapped every ten cycles, instead of one cycle. Thus, the increased switching loss brought by gating pattern swapping can be omitted.

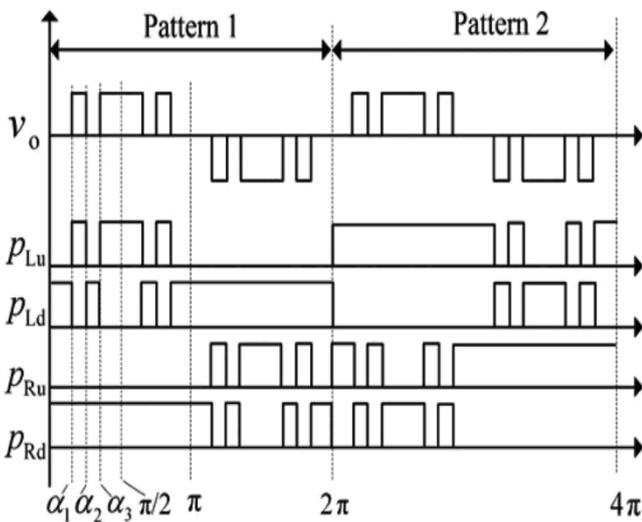
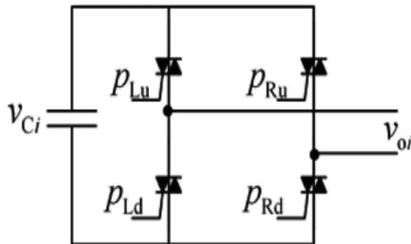


Fig. 4. Modulation Technique

B. Calculation of switching angle

The three switching angles are depicted using α_1 - α_3 . Since the waveform has quarter wave and half wave symmetry, not even harmonics exist. Normalized with respect to dc voltage, the Fourier coefficient is magnitudes of the output voltage of the i^{th} inverter unit is given by,

$$h_i(n) = \left(\frac{4}{n\pi}\right) \sum_{k=1}^3 (-1)^{k+1} \cos(n\alpha_{ik})$$

Where, $n=1,3,5,\dots$ (1)

The first optimization objective is to equalize the inverter units' fundamental output voltages.

$$h_i(1) = \left(\frac{4}{\pi}\right) \sum_{k=1}^3 (-1)^{k+1} \cos(\alpha_{ik}) = M$$

(2)

where,
 $i=1, 2 \dots N$

M =Modulation Index

Another optimization objective is the harmonic distortion

of the synthesized output voltages. The coefficient magnitude of the n th harmonic of the synthesized phase voltage is given by

$$hi(n) = (4/n\pi) \sum_{i=1}^N \sum_{k=1}^3 (-1)^{k+1} \cos(n\alpha_{ik})$$

(3)

The minimizing function of the THD is given by

$$\min F = \sum_{n=3,5,7}^G H(n)^2$$

(4)

Where, $G=2Nk-1$

The linear inequality constraint that the minimization should be subjected to is

$$0 < \alpha_{i1} < \alpha_{i2} < \alpha_{i3} < \frac{\pi}{2}$$

(5)

Using equation (2), (4), (5) switching angles can be calculated using mathematical tool such as MATLAB.

IV. HYBRID CONTROLLER

The operating point changes, select an appropriate method of fuzzy inference method. But the rules for determining the fuzzy controller must be followed in an efficient way. The rule of fuzzy inference rules of the system energy function has been used [3-4]. We can obtain rules by a set of combined methods. If the property adaptive and adjustable being added to the fuzzy system, we can obtain Neuro-Fuzzy system. In all of these systems, parameters belonging to the fuzzy rules can be using the property learning neural networks can be set up in each replicate. Work with other concerned about how the formation of laws and functions, membership and range changes, coefficients will not be output. This means every time parameters set and reach their optimum value. Method proposed here using paired input - output system to produce rules and membership functions is used. System ANFIS parameters can be adaptive neural fuzzy inference consumer ANFIS adaptive network and fuzzy controller to regulate terms of educational performance is quite similar inference system, hybrid algorithm to obtain ANFIS is fuzzy [11] uses membership function parameters. In fact, the hybrid method propagation algorithm for training the minimum square error and system as ANFIS uses fuzzy inference.

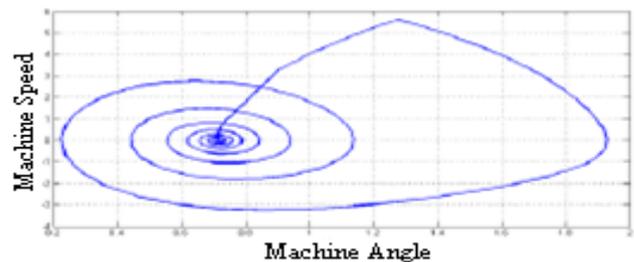


Fig. 5 Graph Page phase system using FC

Equivalent graph form will be observed in Fig. 5. The network is having five layers. First layer: This layer is related to membership functions; Second layer: This layer is related to the formation of

fuzzy rules; Third layer: layer is normalization; Fourth layer: the output of this layer to multiply the output of the third layer in a first order polynomial finds formation; Fifth layer: All statements fourth layer has formed. Trained network and the ANFIS method Controller can work with change-point response is appropriate. This ANFIS controller structure is shown in Fig. 6.

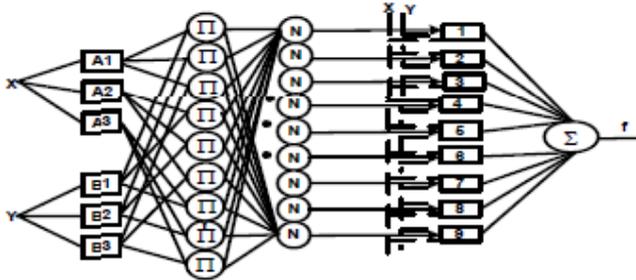


Fig. 6 ANFIS Controller Structure

The input signal controlling the angle of internal R and Z is rapidly changing output signal flow static synchronous compensation injection fits both input vector is to obtain the neural network training patterns, work is under used.

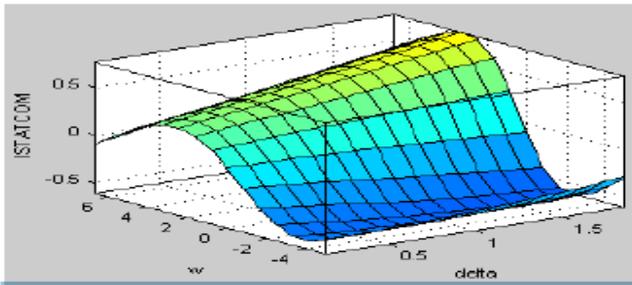


Fig. 7 level curve for the fuzzy controller trained by ANN

Working with these various conditions can be 50 pairs of input patterns would set a bad exit, the 50 patterns can function criteria Lyapunov well they meet. So that each output function of two vectors is input. Neural network using input signals are a system $\times 2$ and $50 \times$ the output of a matrix, respectively 50 educations so that the result obtained by A. Vrdn laws and interval membership functions and controller is finally better response. After learning process for fuzzy control surface curve - according to neural will be obtained. Level curve for the fuzzy controller trained by ANN is shown in Fig. 7.

V. SIMULATION RESULTS

The indirect training strategy of ANN (with $l = 201$, $\sigma_v = 1500$, $\eta_v = 0.2$ and $\Delta w = 0.005$) for transient stability (with $s = 5$) was evaluated for the range of the modulation index, with excellent results in all cases. Fig. 8 shows the obtained switching angles for various values of modulation index ($m \in [0,1]$ with $\Delta m = 0.01$) without BPA.

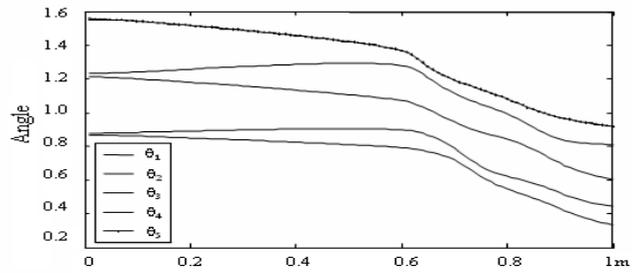


Fig. 8 Switching angles after training phase

Fig. 9 shows the output voltage at various load conditions without controller and Fig. 10 shows the real and reactive power of the system at bus 3 without controller. Fig. 11 shows the voltage at bus 3 by using neural controller. Fig 12 shows the real and reactive power of the system at bus 3 by using neural controller. From the graph it is inferred that transient period is reduced and also voltage is regulated. Reactive power is reduced and active power is improved. By comparing without compensator, the time critical error is reduced in Neural Controller.

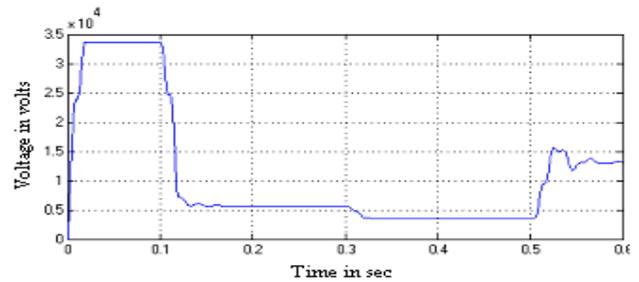


Fig. 9 Output Voltage Waveform at Bus 3 without controller

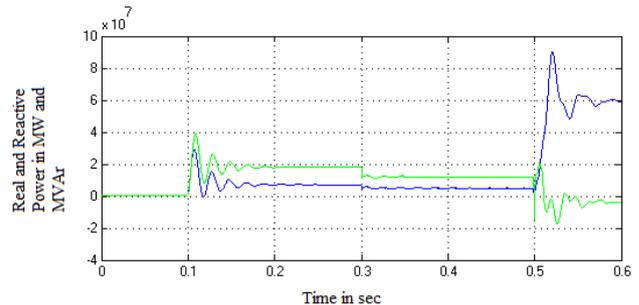


Fig. 10 Real and Reactive at Bus 3 without controller

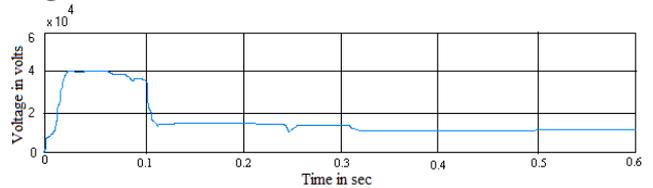


Fig. 11 Output Voltage waveform at Bus 3 with neural control

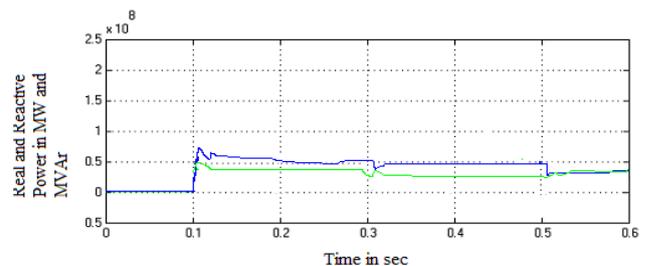


Fig. 12 Real and Reactive Power at Bus 3 with neural control

Fig. 13 shows the voltage at bus 3 by using fuzzy

controller. Fig 14 shows the real and reactive power of the system at bus 3 by using fuzzy controller. From the graph it is inferred that transient period is reduced and also voltage is regulated. Reactive power is reduced and active power is improved.

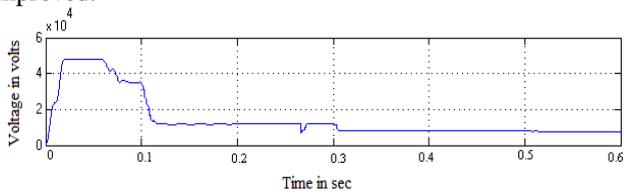


Fig. 13 Output Voltage waveform at Bus 3 with fuzzy control

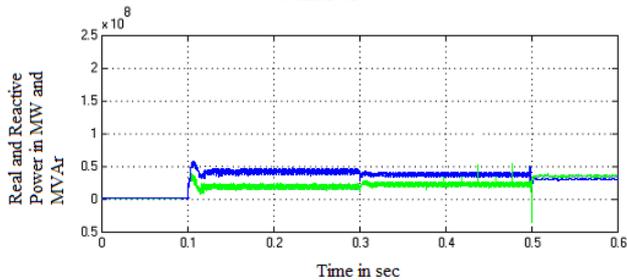


Fig. 14 Real and Reactive Power at Bus 3 with fuzzy Control

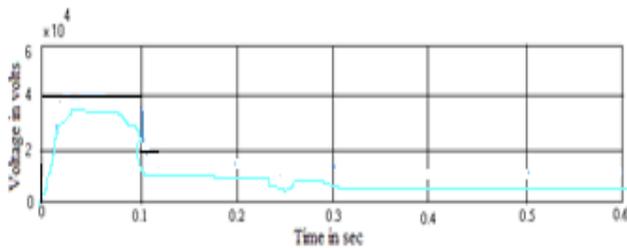


Fig. 15 Output Voltage waveform at Bus 3 with hybrid controller

Fig. 15 shows the voltage at bus 3 by using hybrid controller. Fig. 16 shows the real and reactive power of the system at bus 3 by using hybrid controller. From the graph it is inferred that transient period is reduced and also voltage is regulated. Reactive power is reduced and active power is improved. By comparing without compensator, the time critical error is reduced in hybrid controller.

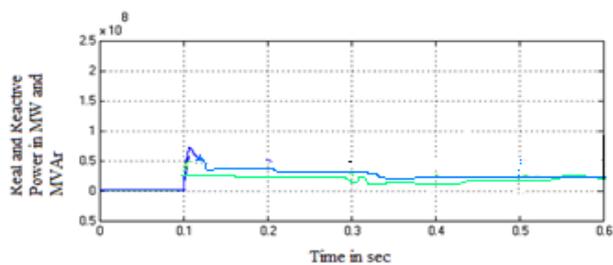


Fig. 16 Real and Reactive Power at Bus 3 with hybrid controller

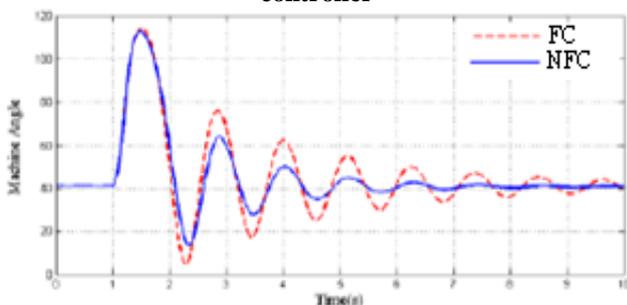


Fig. 17 The internal angle of generator

Compared to without controller case, hybrid controller improves transient stability for a network is investigated. Synchronous static in the middle of the line has been a short circuit at the time generator is applied and after bleaching for 200 ms pure is performing. Simulation graph of generator internal angle, for each STATCOM system speed, flow graph and STATCOM flow is shown in Fig. 17, Fig. 18 and Fig. 19, Fig. 20 respectively. Simulation results show that controlling damping oscillations could FC proposal in comparison with control hybrid NFC System after short circuit increase.

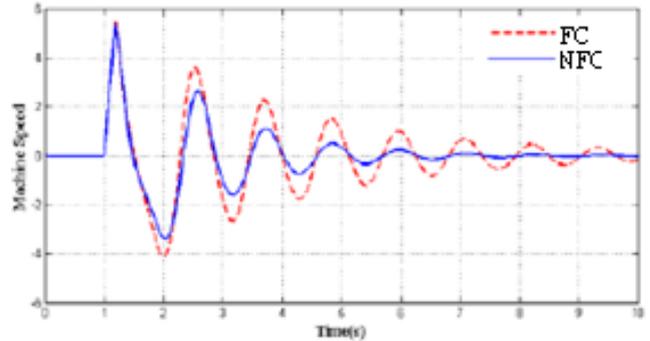


Fig. 18 generator speed changes

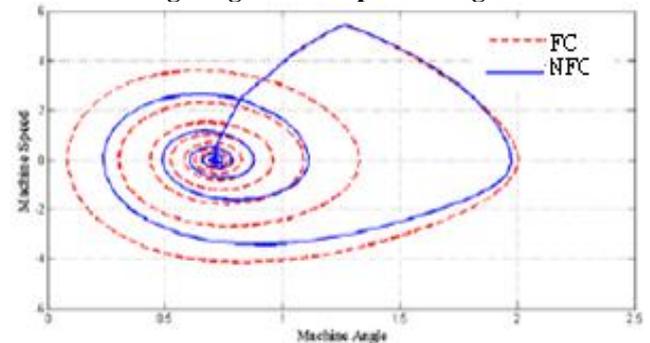


Fig. 19 Graph Page phase system

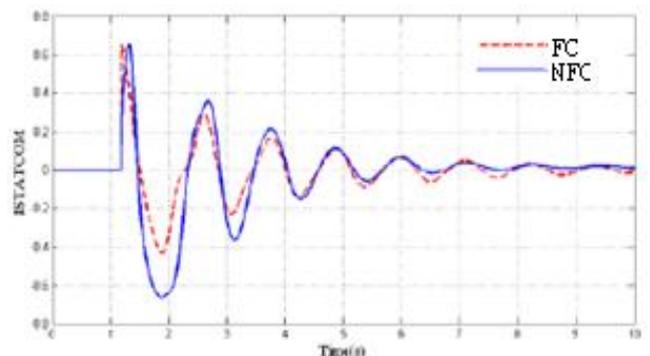


Fig. 20 STATCOM flow

Table I. Comparison Of Time Critical

Controller	Without Controller	FC	NC	Hybrid NFC
Time Critical (Seconds)	1/185	1/205	1/198	1/219

Table 1 shows the amount of time to critical error in three cases without controller, FC and hybrid NFC. Comparing the three time drive controller, transient stability improvement is evident in hybrid NFC.

VI. CONCLUSION

A hybrid controller is designed based on energy function Lyapunov, for compensating the effect of synchronous after the system disturbance. For switching the device, swapping technique is adopted. The scheme of gating-pattern swapping among the various devices can equalize device current stresses. A multilevel optimal modulation strategy was proposed for STATCOM, is incorporated in system line. So the system is easily balanced. Hybrid is employed to enhance the transient stability. It is inferred from the graph transient is reduced using hybrid. Finally the proposed system reduces the critical time error.

APPENDIX

For STATCOM

Rated Power = 100 MVA

Rated voltage= 138 kV

Interface inductor (L) = 2.86 mH

Resistance (Rs) = 0.0898 Ω

For grid

Rated Voltage: 230 kV

Short Circuit Capacity: 10000 MVA

For Power Transformer (Y/Y)

Rated Voltage 220 kV/33 kV

Rated Power: 300 MVA

For Coupling Transformer (Y/Y)

Rated Voltage 138 kV/230 kV

Rated Power: 100 MVA

Three Phase Load

Load 1:

P= 100 MW

Q= 80 MVA

Load 2:

P= 70 MW

Q= 50 MVA

Load 3:

P= 60 MW

Q= 40 MVA

REFERENCES

1. J. S. Lai and F. Z. Peng, Multilevel converters—A new breed of power converters, *IEEE Trans. Ind. Appl.*, Vol. 32, no. 3, May/June. 1996, pp. 509–517.
2. F. Z. Peng, J. -S. Lai, J. W. McKeever, and J. VanCoevering, A multilevel VSI with separate DC sources for static VAR generation, *IEEE Trans. Ind. Appl.*, Vol. 32, no. 5, Sep./Oct. 1996, pp. 1130–1138.
3. P. M. Bhagwat and V. R. Stefanovic, Generalized structure of a multilevel PWM inverter, *IEEE Trans. Ind. Appl.*, Vol. 19, Nov./Dec. 1983, pp. 1057–1069.
4. M. Marchesoni and M. Mazzucchelli, Multilevel converter for high power ac drives: A review, *IEEE Symp. Indl. Electrs.*, 1993, pp.38–43.
5. H. Akagi, The state-of-the-art of power electronics in Japan, *IEEE Trans. Power Electron.* Vol. 13, Mar. 1998, pp. 345–356.
6. G. Carrara, S. Gardella, M. Marchesoni, R. Salutati, and G. Sciuotto, A new multilevel PWM method: A theoretical analysis, *IEEE Trans. Power Electron.*, Vol. 7, July 1992, pp. 497–505.
7. B. Mwinjiwiwa, Z. Wolanski, and B. T. Ooi, Microprocessor-implemented SPWM for multi converters with phase-shifted triangle carriers, *IEEE Trans. Ind. Appl.* Vol. 34, May/June 1998, pp. 487–494.
8. S. Ogasawara, J. Takagaki, H. Akagi, and A. Nabae, A novel control scheme of a parallel current-controlled PWM inverter, *IEEE Trans. Ind. Applicat.*, Vol. 28, Sept. / Oct. 1992, pp. 1023–1030.

9. F. Ueda, K. Matsui, M. Asao, and K. Tsuboi, Parallel-connections of PWM inverters using current sharing reactors, *IEEE Trans. Power Electron.* Vol. 10, Nov. 1995, pp. 673–679.
10. D. Daniolos, M.K. Darwish and P. Mehta, “Optimised PWM inverter control using Artificial Neural Networks”, *IEE 1995 Electronics Letters Online*, No. 19951186, 14 August 1995, pp. 1739–1740.
11. A.M. Trzynadlowski and S. Legowski, “Application of Neural Networks to the Optimal Control of Three-Phase Voltage-Controlled Inverters”, *IEEE Transactions on Power Electronics*, Vol.9, No.4, July 1994, pp.397–402.
12. M. Mohaddes, A.M. Gole and P.G. McLaren, “A Neural Network Controlled Optimal pulse-width modulated STATCOM”, *IEEE Transactions on Power Delivery*, Vol. 14, Issue:2, April 1999, pp.481–488.
13. S. Mori, et al., Development of a Large Static Var Generator Using Self-Commutated Inverters for Improving Power Systems Stability, *IEEE Trans. Power Delivery*, Vol. 8, No.1, Feb.1993, pp. 371–377.
14. N. Seki, H. Uchino, Converter Configurations and Switching Frequency for GTO Reactive Power Compensator, *IEEE Trans. on Industry Applications*, Vol. 33, No. 4, July/August 1997.
15. S.A. Al-Mawsawi, Fuzzy Control and Dynamic Performance of STATCOM, *IETECH J. of Elec. Analysis*, 2007, Vol.1, No. 2, pp. 104–115.
16. A. Ajami, S.H. Hosseini, Application of a Fuzzy Controller for Transient Stability Enhancement of AC Transmission System by STATCOM, *Intl. Joint Conf. ICASE*, October 2002, pp. 6059 – 6063.

AUTHOR PROFILE



Dhal P.K. born in Jajpur, Orissa and received his M.E. degree (power systems) from Madurai Kamaraj University, Madurai. He is currently pursuing Ph.D degree in sathyabama University, Chennai. He is currently working as Assistant professor in Electrical & Electronics Engineering Department at Vel Tech DR.RR&DR.SR Technical University, Avadi, Chennai. He is member in ISTE & IEEE.



C. Christober Asir Rajan born on 1970 and received his B.E. (Distn.) degree (Electrical and Electronics) and M.E. (Distn.) degree (Power System) from the Madurai Kamaraj University (1991 & 1996), Madurai, India. And he received his postgraduate degree in DI.S. (Distn.) from the Annamalai University, Chidambaram (1994). He received his Ph.D in Power System from Anna University (2001-2004), Chennai, India. He published technical papers in International & National Journals and Conferences. He is currently working as Associate Professor in the Electrical Engineering Department at Pondicherry Engineering College,

Pondicherry, India. His area of interest is power system optimization, operational planning and control. He acquired Member in ISTE and MIE in India and Student Member in Institution of Electrical Engineers, London.